

**Method for Calibrating Analog Controlling, Electrically  
Actuatable Hydraulic Valves**

The invention relates to a method according to the preamble of claim 1 and a device according to claim 7.

It is known in the art to employ analog controlling, electrically actuatable hydraulic valves for the purpose of hydraulic pressure control in ABS control devices for motor vehicle brake systems, but also in so-called driving dynamics controllers equipped with additional functions such as ESP, etc.

So-called analog/digital valves, are used in more recent generations of hydraulic control devices. An analog/digital valve is a switching valve that is so operated that it inheres analog control characteristics. This valve is designed in a manner that it can be operated both in analog and digital ways.

EP 0 813 481 B1 (P 7565) discloses a method for detecting the operating point of the valve, in particular for determining the pressure ratios from the current variation of the valve actuating current.

In principle, the coil current can be used to adjust the pressure gradient built up by the valve. However, a complicated calibration is necessary to this end, as is known. As described e.g. in WO 01/98124 A1 (P 9896), characteristic curves for the valves are established for

this purpose, and nominal currents are adjusted which are calculated by means of the characteristic curves depending on the desired pressure gradient. Consequently, the volume flow  $Q$  with respect to characteristic line  $f$  depends on the differential current  $\Delta p$  and on current  $I$ .

DE 102 214 56 A1 discloses a calibration method for analogized inlet and separating valves according to the preamble of claim 1. The calibration method described in this publication does not manage without the use of a so-called testing rod, therefore necessitating a testing device that has a correspondingly sophisticated design for depressing the brake pedal.

It is, however, complicated and disadvantageous to prepare individual calibration data or characteristic curves for each valve during manufacture, for example, by manually fitting the brake control unit into a device comprising a testing rod. It is further disadvantageous when e.g. the electronics of an electrohydraulic device, which contains these valves, must be exchanged at a later point of time for maintenance purposes. The calibration data memorized therein will usually get lost in this case. In view of the above, the object to be achieved involves providing a method, which allows preparing correspondingly suitable calibration data or characteristic curves in a simpler fashion.

This object is achieved by the method according to claim 1.

The calibration of the invention is carried out by means of the device automatically by using the hydraulic energy of the pressurization unit controlled by extraneous force (for example, a piston pump driven by a motor). The calibration is preferably performed only after the production of the

valve or the electrohydraulic device in the object into which the valve or the electrohydraulic device is mounted. Thus, it is possible to perform the calibration e.g. only after fitting the control unit into a motor vehicle.

This method entails considerably less costs than preparing calibration data at the assembly line, because a transfer of the calibration data into the electronic control connected to the valve is no longer necessary.

Preferably, the electrohydraulic control device in which the valves are mounted comprises several hydraulic pressure control circuits, which can be separately driven by means of inlet and outlet valves. A brake cylinder is associated with each circuit in a particularly preferred manner. Regarding the example of a brake unit, each pressure control circuit is allocated to a motor vehicle wheel.

The electrohydraulic control device comprises on the inlet side preferably one pressure sensor, e.g. in the area of the master cylinder (Thz - tandem master cylinder).

Several or all of the circuits are preferably equipped with further ,circuit pressure sensors', which enable individual pressure measurement in each hydraulic circuit.

A coil current which is essentially associated with a determined differential pressure can be defined in the solenoid valves to be calibrated according to the invention, these valves concerning normally open inlet valves of a brake control unit in particular.

In addition, the method can be used favorably to monitor the proper functioning of the device.

After the installation of the brake control unit, the described calibration routine is expediently carried out one time during the first initiation or with each ignition cycle.

Preferably, a motor vehicle into which the brake unit is especially mounted is at standstill while the calibration routine is performed.

It is favorably monitored during the process whether a determined predefined maximum time is not exceeded when filling the pressure accumulator.

It is furthermore favorable that it is monitored whether the established characteristic curve or the established calibration data lie within a predefined range of validity.

Further preferred embodiments can be seen in the sub claims and the following description of the Figures.

Hereinbelow, the invention will be explained in detail with reference to an example.

In the drawings:

Figure 1 is a schematic view of a brake unit with analog actuatable valves, and

Figure 2 shows a diagram for illustrating the pressure variations and the valve current.

Referring to Figure 1, tandem master cylinder 5 is connected to valve block 6 of an electronic motor vehicle brake system. Electronic unit 7 comprises a microcontroller system used to electronically control or measure the actuators and sensors provided in the valve block. Valve block 6 comprises two brake circuits I and II. Each brake circuit comprises two wheel pressure circuits with respectively one inlet valve 3 and one outlet valve 4. Reference numeral 2 designates a normally open separating valve and reference numeral 8 designates a normally closed electronic change-over valve. An inlet pressure sensor 9 is positioned in the hydraulic line leading to the master cylinder 5. One or more pressure sensors 10, 10', 10'', 10''' are arranged in the wheel pressure circuits. Pump 1 is used for the independent pressure increase, such as in the TCS or ESP case.

For calibration, valve 2 is closed and valve 8 opened initially in a first step. Pump 1 is activated. Valve 3 is closed after pressure buildup of roughly 5 bar in the pressure circuit A (calibration circuit). Valve 3' in circuit B remains open until a pressure of roughly 180 bar is reached in circuit B. The pressure in circuit A is greater zero to prevent undesirable effects (e.g. cavitations) during the actual calibration.

In the next step, the pump is switched off and valve 8 is closed. The pressure in circuit B is then initially shut in similar to a pressure accumulator.

The further process will now be explained referring to Figure 2. The pump is switched off at time t1. The pressure in the 'accumulator wheel' B amounts to 180 bar approximately. At time t2, the valve current of the valve 3 under calibration is increased at the 'calibration wheel' A

to such an extent that the valve is tightly closed. Subsequently (starting with  $t_3$  to  $t_4$ ), the current is slowly decreased. The valve meanwhile opens, at point ' $O_0$ ', so that the pressure drops in the accumulator wheel A. Accordingly, the pressure rises in the calibration wheel B in the area ' $O$ '. When a differential pressure ( $P_B - P_A$ ) of 140 bar is reached, the reference point  $SP_1$  is acquired and stored. At point  $SP_1$ , valve 3 is closed again due to a steep current increase (flank  $F_1$ ). The pressure variation is stopped hereby. Subsequent thereto, pressure decrease is used to search for point  $O_1$ , where the valve is just bringing about a change in pressure again. For example, this can be detected by monitoring that a predefined threshold value is not reached. The opening current at point  $O_1$  is memorized as being linked to the pressure at reference point  $SP_1$ . Thereafter, the method is continued in a corresponding fashion for measuring further reference points ( $SP_2, O_2$ ), ( $SP_3, O_3$ ), ..., ( $SP_n, O_n$ ). A calibration curve  $\Delta P(I)$  for valve 3 is obtained.

The method is then repeated for the remaining wheel pressure circuits B to D, and an adjacent wheel pressure circuit is used as an accumulator circuit in each case. It is this way possible to measure calibration curves for all inlet valves.

For example, the method can be secured in addition by checking whether

- all pressure sensors furnish plausible signals,
- the vehicle is at standstill during the calibration time,
- a maximum time for pressure increase is not exceeded,
- the characteristic curve found lies within certain limits (e.g. maximum characteristic curve, minimum characteristic curve, minimum and maximum gradient).

It is furthermore expedient to protect the calibration data or the data of the characteristic curves by check sums.